

There will come soft rains and the smell of the ground,
And swallows circling with their shimmering sound;
And frogs in the pools singing at night,
And wild plum trees in tremulous white;

Robins will wear their feathery fire
Whistling their whims on a low fence-wire,
And not one will know of the war, not one
Will care at last when it is done.

Chapter 5: The Rigid Body Equations of Motion

Section 1. Angular Momentum and Kinetic Energy of Motion about a Point

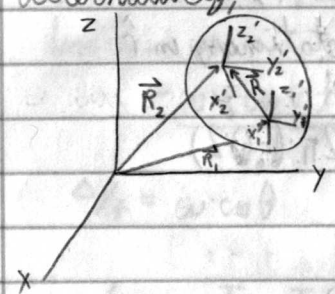
Chasles' Theorem (Chapter 4, Section 6) suggests that we should be able to split rigid body motion into a translational and rotational component. We have six coordinates to describe motion: 3 cartesian coordinates for translation and 3 Euler angles for rotation. If we set the origin at the center-of-mass, then we can divide the angular momentum and the kinetic energy into a translational and rotational component, like so

$$\vec{L} = \vec{R} \times M\vec{v} + \sum_i \vec{r}_i' \times \vec{p}_i' \quad (1.28)$$

$$\vec{T} = \frac{1}{2} M v^2 + \frac{1}{2} \sum_i m_i v_i'^2 \quad (1.31)$$

In order to obtain angular momentum and kinetic energy of motion about some body point, we want to first show that the rotation angle of a rigid body displacement is independent of the origin. We can show this by remembering that all particles of the body move and rotate together.

Alternatively,



$$\begin{aligned} \vec{R}_2 &= \vec{R}_1 + \vec{R} \\ \left(\frac{d\vec{R}_2}{dt}\right)_s &= \left(\frac{d\vec{R}_1}{dt}\right)_s + \left(\frac{d\vec{R}}{dt}\right)_s \\ &= \left(\frac{d\vec{R}_1}{dt}\right)_s + \left(\frac{d\vec{R}}{dt}\right)_r + \vec{\omega}_1 \times \vec{R} \\ &= \left(\frac{d\vec{R}_1}{dt}\right)_s + \vec{\omega}_1 \times \vec{R} \end{aligned} \quad (4.86)$$

$$\begin{aligned} \vec{R}_1 &= \vec{R}_2 - \vec{R} \\ \left(\frac{d\vec{R}_1}{dt}\right)_s &= \left(\frac{d\vec{R}_2}{dt}\right)_s - \vec{\omega}_2 \times \vec{R} \\ \vec{\omega}_1 \times \vec{R} - \vec{\omega}_2 \times \vec{R} &= 0 \\ (\vec{\omega}_1 - \vec{\omega}_2) \times \vec{R} &= 0 \\ \Rightarrow \vec{\omega}_1 &= \vec{\omega}_2 \end{aligned}$$

Not one would mind, neither bird nor tree
If mankind perished utterly;
And Spring herself, when she woke at dawn,
Would scarcely know that we were gone.

- Sara Teasdale (There will come soft rains, 1920)

From (1.28), if we keep one point stationary ($\vec{v} = 0$),

$$\vec{L} = m_i (\vec{r}_i \times \vec{v}_i) \quad (5.1)$$

$$\vec{v}_i = \vec{\omega} \times \vec{r}_i \quad (5.2)$$

$$\begin{aligned} \vec{L} &= m_i \vec{r}_i \times (\vec{\omega} \times \vec{r}_i) \\ &= m_i [\vec{\omega} (\vec{r}_i \cdot \vec{r}_i) - \vec{r}_i (\vec{r}_i \cdot \vec{\omega})] \\ &= m_i [\vec{\omega} r_i^2 - \vec{r}_i (\vec{r}_i \cdot \vec{\omega})] \end{aligned} \quad (5.3)$$

Remembering the implicit summation

$$\begin{aligned} L_x &= m_i [\omega_x r_i^2 - \omega_x x_i^2 - x_i y_i \omega_y - x_i z_i \omega_z] \\ &= \omega_x m_i (r_i^2 - x_i^2) - \omega_y m_i x_i y_i - \omega_z m_i x_i z_i \end{aligned} \quad (5.4)$$

$$L_y = \omega_y m_i (r_i^2 - y_i^2) - \omega_x m_i y_i x_i - \omega_z m_i y_i z_i$$

$$L_z = \omega_z m_i (r_i^2 - z_i^2) - \omega_x m_i z_i x_i - \omega_y m_i z_i y_i$$

$$L_x = I_{xx} \omega_x + I_{xy} \omega_y + I_{xz} \omega_z \quad (5.5)$$

$$I_{xx} = m_i (r_i^2 - x_i^2) \quad (5.6)$$

$$I_{xy} = -m_i x_i y_i \quad (5.7)$$

$$I_{xz} = -m_i x_i z_i$$

The matrix \vec{I} (uh oh, not identity matrix, something, something, context) is the inertia tensor. The diagonal terms are the moment of inertia coefficients, and the off-diagonal terms are the products of inertia. The components can be written as

$$I_{jk} = \int_V \rho(\vec{r}) (r^2 \delta_{jk} - x_j x_k) dV \quad (5.8)$$

(5.5) can be rewritten as

$$\vec{L} = \vec{I} \vec{\omega} \quad (5.9)$$

Section 2. Tensors.

We mention tensors in the previous section. In a Cartesian three-dimensional space, an N^{th} -rank tensor has 3^N components, and under an orthogonal transformation $\vec{T}' = \vec{A} \vec{T}$,

$$T'_{ijk}(\vec{x}') = a_{i\ell} a_{jm} a_{kn} T_{\ell mn}(\vec{x}) \quad (5.10)$$

A scalar is a tensor of zero rank, a vector is a tensor of first rank, and a square matrix (assuming it satisfies (5.10)) is a tensor of second rank.

Section 3. The Inertia Tensor and the Moment of Inertia

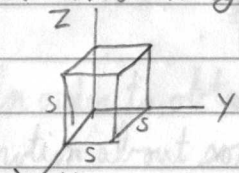
$$\begin{aligned}
 (1.2) \quad T &= \frac{1}{2} m_i v_i^2 \\
 (5.2) \quad &= \frac{1}{2} m_i \vec{v}_i \cdot (\vec{\omega} \times \vec{r}_i) \\
 &= \frac{\vec{\omega}}{2} \cdot m_i (\vec{r}_i \times \vec{v}_i) \\
 &= \vec{\omega} \cdot \frac{1}{2} \vec{I} = \frac{1}{2} \vec{I} \vec{\omega} \quad (5.17)
 \end{aligned}$$

where I is a scalar, defined as

$$I = \hat{n} \cdot \vec{I} \cdot \hat{n} = m_i [r_i^2 - (\vec{r}_i \cdot \hat{n})^2] \quad (5.18)$$

compare to (5.8).

(7.2) As an example, consider we have a cube of uniform mass density μ and side length s with pivot at a corner



Using (5.8)

$$\begin{aligned}
 (5.2) \quad I_{11} = I_{22} = I_{33} &= \int_0^s \int_0^s \int_0^s \mu (x^2 + x_2^2 + x_3^2 - x^2) dx_1 dx_2 dx_3 \\
 &= \mu \int_0^s \int_0^s \int_0^s (x_2^2 + x_3^2) dx_1 dx_2 dx_3 \\
 &= \mu s \int_0^s \int_0^s (x_2^2 + x_3^2) dx_2 dx_3 \\
 &= \mu s \int_0^s (\frac{1}{3} s^3 + s x_3^2) dx_3 \\
 &= \mu s (\frac{1}{3} s^4 + \frac{1}{3} s^4) = \frac{2}{3} \mu s^5
 \end{aligned}$$

(8.2) Off-diagonal terms are all equal

$$\begin{aligned}
 (8.2) \quad &= -\mu \int_0^s \int_0^s \int_0^s (-x_1 x_2) dx_1 dx_2 dx_3 \\
 (9.2) \quad &= -\mu \int_0^s \int_0^s \frac{1}{2} s^2 x_2 dx_2 dx_3 \\
 &= -\frac{1}{2} \mu s^2 \int_0^s \frac{1}{2} s^2 dx_3 \\
 &= -\frac{1}{4} \mu s^5
 \end{aligned}$$

$$I = \frac{2}{3} (\mu s^5) \begin{bmatrix} | & -\frac{3}{8} & -\frac{3}{8} \\ -\frac{3}{8} & | & -\frac{3}{8} \\ -\frac{3}{8} & -\frac{3}{8} & | \end{bmatrix} = \frac{2}{3} \mu s^5 \begin{bmatrix} | & \alpha & \alpha \\ \alpha & | & \alpha \\ \alpha & \alpha & | \end{bmatrix}$$

Section 4. The Eigenvalues of the Inertia Tensor

We saw that the inertia tensor is symmetric,

$$I_{xy} = I_{yx} \quad (5.24)$$

The eigenvalues of the inertia tensor are referred to as the components of the principal moment of inertia tensor.

In the previous example:

$$\begin{aligned}
 \begin{bmatrix} 1-\lambda & \alpha & \alpha \\ \alpha & 1-\lambda & \alpha \\ \alpha & \alpha & 1-\lambda \end{bmatrix} &= (1-\lambda)[(1-\lambda)^2 - \alpha^2] - \alpha[\alpha(1-\lambda) - \alpha] + \alpha[\alpha^2 - \alpha(1-\lambda)] \\
 &= (1-\lambda)^3 - 3\alpha^2(1-\lambda) + 2\alpha^3 \\
 &= (1-\lambda - \alpha)^2 (1-\lambda + 2\alpha) = 0
 \end{aligned}$$

$$\lambda_1 = \frac{1}{4}$$

$$\lambda_2 = \lambda_3 = \frac{11}{8}$$

$$|\lambda_1\rangle: \begin{bmatrix} \frac{3}{4} & -\frac{3}{8} & -\frac{3}{8} \\ -\frac{3}{8} & \frac{3}{4} & -\frac{3}{8} \\ -\frac{3}{8} & -\frac{3}{8} & \frac{3}{4} \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$|\lambda_1\rangle = \frac{1}{\sqrt{3}} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$$

$$|\lambda_2\rangle: \begin{bmatrix} -\frac{3}{8} & -\frac{3}{8} & -\frac{3}{8} \\ -\frac{3}{8} & -\frac{3}{8} & -\frac{3}{8} \\ -\frac{3}{8} & -\frac{3}{8} & -\frac{3}{8} \end{bmatrix} \begin{bmatrix} a \\ b \\ c \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$|\lambda_2\rangle = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ -1 \\ 0 \end{bmatrix}$$

$$|\lambda_3\rangle = \frac{1}{\sqrt{6}} \begin{bmatrix} -1 \\ -1 \\ 2 \end{bmatrix}$$

Section 5. Solving Rigid Body Problems and the Euler Equations of Motion

$$T = \frac{1}{2} M v^2 + \frac{1}{2} I \omega^2 \quad I = \sum m_i r_i^2$$

The kinetic energy can be broken up into a translational and a rotational component

$$L = L_c(q, \dot{q}) + L_b(q, \dot{q})$$

$$\left(\frac{\partial L}{\partial t}\right)_s = \left(\frac{\partial L}{\partial t}\right)_b + \vec{\omega} \times \vec{L}$$

Compare to (4.82)

$$I_1 \dot{\omega}_1 - \omega_2 \omega_3 (I_2 - I_3) = N_1$$

$$I_2 \dot{\omega}_2 - \omega_3 \omega_1 (I_3 - I_1) = N_2$$

$$I_3 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) = N_3$$

$$(5.39)$$

Euler's equations of motion for a rigid body with one point fixed

Section 6. Torque-Free Motion of a Rigid Body

If there are no outside forces, Euler's equations reduce to

$$I_1 \dot{\omega}_1 = \omega_2 \omega_3 (I_2 - I_3)$$

$$I_2 \dot{\omega}_2 = \omega_3 \omega_1 (I_3 - I_1)$$

$$I_3 \dot{\omega}_3 = \omega_1 \omega_2 (I_1 - I_2)$$

$$(5.40)$$

Define a vector

$$\vec{\rho} = \frac{\vec{\omega}}{\sqrt{2T}}$$

and a function

$$F(\rho) = \vec{\rho} \cdot \vec{I} \cdot \vec{\rho} = \rho_i^2 I_i$$

$$(5.42)$$

If F is constant, it traces out an ellipsoid.

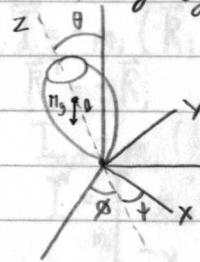
$$\nabla_{\rho} F = \sqrt{2T} \vec{I}$$

$$(5.43)$$

$$\vec{\rho} \cdot \vec{I} / L = \sqrt{2T} / L$$

$$(5.44)$$

Section 7. The Heavy Symmetrical Top with One Point Fixed



$\dot{\psi}$ = rotation about body axis z

$\dot{\phi}$ = rotation of z about z'

$\dot{\theta}$ = bobbing up and down of z relative to z'

In general, $\dot{\psi} \gg \dot{\theta} \gg \dot{\phi}$ & $I_1 = I_2 \neq I_3$

Euler's equations become

$$I_1 \dot{\omega}_1 + \omega_2 \omega_3 (I_3 - I_2) = N_1$$

$$I_2 \dot{\omega}_2 + \omega_1 \omega_3 (I_1 - I_3) = N_2$$

$$I_3 \dot{\omega}_3 = N_3$$

Using (4.87),

$$T = \frac{1}{2} I_1 (\dot{\omega}_1^2 + \dot{\omega}_2^2) + \frac{1}{2} I_3 \dot{\omega}_3^2$$

$$= \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) + \frac{1}{2} I_3 (\dot{\psi} + \dot{\phi} \cos \theta)^2 \quad (5.50)$$

$$V = -M \vec{R} \cdot \vec{g}$$

$$= M g l \cos \theta \quad (5.51)$$

$$L = \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\phi}^2 \sin^2 \theta) + \frac{1}{2} I_3 (\dot{\psi} + \dot{\phi} \cos \theta)^2 - M g l \cos \theta \quad (5.52)$$

Since θ & ψ do not show up in the Lagrangian,

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\theta}} \right) - \frac{\partial L}{\partial \theta} = 0$$

$$I_1 \dot{\phi} \sin^2 \theta + I_3 (\dot{\psi} + \dot{\phi} \cos \theta) \cos \theta = 0$$

$$I_1 \dot{\phi} \sin^2 \theta + I_3 \omega_3 \cos \theta = I_1 b \quad (5.54)$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\psi}} \right) - \frac{\partial L}{\partial \dot{\psi}} = 0$$

$$I_3 (\dot{\psi} + \dot{\phi} \cos \theta) = I_3 \omega_3 = I_1 a \quad (5.53)$$

$$I_1 \dot{\phi} \sin^2 \theta + I_1 a \cos \theta = I_1 b$$

$$\dot{\phi} = \frac{b - a \cos \theta}{\sin^2 \theta}$$

$$(5.57)$$

$$I_3 \dot{\psi} = I_1 a - I_3 \dot{\theta} \cos \theta$$

$$\dot{\psi} = \frac{I_1 a}{I_3} - \frac{b - a \cos \theta}{\sin^2 \theta} \dot{\theta} \quad (5.58)$$

$$E = \frac{1}{2} I_1 (\dot{\theta}^2 + \dot{\psi}^2 \sin^2 \theta) + \frac{1}{2} I_3 \omega_3^2 + Mgl \cos \theta \quad (5.55)$$

$$E - \frac{I_3 \omega_3^2}{2} = \frac{I_1 \dot{\theta}^2}{2} + \frac{I_1 (b - a \cos \theta)^2}{2 \sin^2 \theta} + Mgl \cos \theta \quad (5.59)$$

which is the one-dimensional problem with

$$V'(\theta) = \frac{I_1}{2} \left(\frac{b - a \cos \theta}{\sin \theta} \right)^2 + Mgl \cos \theta \quad (5.60)$$

If we define the four constants of motion as

$$\alpha = \frac{2E - I_3 \omega_3^2}{I_1} \quad (5.61)$$

$$\beta = \frac{2Mgl}{I_1}$$

$$a = \frac{p_\psi}{I_1}$$

$$b = \frac{p_\theta}{I_1} \quad (5.62)$$

$$\alpha = \dot{\theta}^2 + \frac{(b - a \cos \theta)^2}{\sin^2 \theta} + \beta \cos \theta \quad (5.63)$$

let $u = \cos \theta$

$$\dot{u} = -\dot{\theta} \sin \theta$$

$$\alpha = \frac{\dot{u}^2}{\sin^2 \theta} + \frac{(b - a u)^2}{\sin^2 \theta} + \beta u \quad (5.64)$$

$$\sin^2 \theta (\alpha - \beta u) = \dot{u}^2 + (b - a u)^2$$

$$k^2 = (1 - u^2) (\alpha - \beta u) - (b - a u)^2$$

$$t = \int_{u(0)}^{u(t)} \frac{du}{\sqrt{(1 - u^2) (\alpha - \beta u) - (b - a u)^2}} \quad (5.65)$$

Derivations. 1. $\vec{I} = -m_i (\vec{R}_i)^2$ antisymmetric

$$I_{\rho\sigma} = m_i (\delta_{\rho\sigma} r_i^2 - r_{i\rho} r_{i\sigma}) \quad (5.22)$$

$$\vec{I} = \begin{bmatrix} -x_2^2 + x_3^2 & -x_1 x_2 & -x_1 x_3 \\ -x_2 x_1 & x_1^2 + x_3^2 & -x_2 x_3 \\ -x_3 x_1 & -x_2 x_2 & x_2^2 + x_3^2 \end{bmatrix}$$

$$(\vec{R}_i)^2 = \begin{bmatrix} 0 & x_3 & -x_2 \\ -x_3 & 0 & x_1 \\ x_2 & -x_1 & 0 \end{bmatrix} \begin{bmatrix} 0 & x_3 & -x_2 \\ -x_3 & 0 & x_1 \\ x_2 & -x_1 & 0 \end{bmatrix} = \begin{bmatrix} -x_3^2 - x_2^2 & x_1 x_2 & x_1 x_3 \\ -x_1 x_2 & -x_3^2 - x_1^2 & x_2 x_3 \\ x_1 x_3 & x_2 x_3 & -x_2^2 - x_1^2 \end{bmatrix}$$

$$\vec{I} = -m_i (\vec{R}_i)^2$$

$$2. \vec{I} = m_i (\vec{r}_i \times \hat{n}) \cdot (\vec{r}_i \times \hat{n}) = m_i [(\vec{r}_i \cdot \vec{r}_i)(\hat{n} \cdot \hat{n}) - (\vec{r}_i \cdot \hat{n})(\hat{n} \cdot \vec{r}_i)] = m_i [r_i^2 - (\vec{r}_i \cdot \hat{n})^2] \quad (5.18)$$

$$3. T = \frac{1}{2} m_i v_i^2$$

$$\frac{dT}{dt} = m_i v_i \frac{dv_i}{dt} = m_i (\vec{\omega} \times \vec{r}_i) \cdot \frac{d\vec{v}_i}{dt}$$

$$= m_i \vec{\omega} \cdot \left(\vec{r}_i \times \frac{d\vec{v}_i}{dt} \right) = \vec{\omega} \cdot \left(m_i \vec{r}_i \times \frac{d\vec{v}_i}{dt} \right) = \vec{\omega} \cdot \vec{N}$$

$$4. \vec{N} = \vec{r} \times \vec{F} = \vec{r} \times m \frac{d\vec{v}}{dt}$$

$$4. \frac{d}{dt} \left(\frac{\partial T}{\partial \dot{\phi}} \right) - \frac{\partial T}{\partial \phi} = N$$

$$T = \frac{1}{2} I_1 \omega_1^2$$

$$\frac{d}{dt} \left(I_1 \omega_1 \frac{d\omega_1}{dt} \right) - \frac{\partial}{\partial \phi} \left(\frac{I_1 \omega_1^2}{2} \right) = N$$

$$\frac{d}{dt} \left(I_1 \omega_1 \frac{d\omega_1}{dt} \right) - \frac{I_1}{2} \cdot 2\omega_1 \frac{d\omega_1}{dt} = N$$

From (4.87),

$$\frac{d\omega_1}{dt} = 0 \quad \frac{d\omega_2}{dt} = \omega_1$$

$$\frac{d\omega_2}{dt} = 0 \quad \frac{d\omega_3}{dt} = -\omega_1$$

$$\frac{d\omega_3}{dt} = 1 \quad \frac{d\omega_3}{dt} = 0$$

$$\frac{d}{dt} (I_3 \omega_3) - I_1 \omega_1 \omega_2 + I_2 \omega_2 \omega_1 = N_3$$

$$I_3 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) = N_3$$

By permuting x, y, and z, we can return the rest of (5.39)

5. In (5.39), I_i is a constant

$$I \frac{d\omega_i}{dt} = \frac{d(I\omega_i)}{dt} - \omega_j \frac{dI}{dt}$$

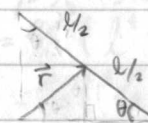
$$u = I \quad v = \omega_j$$

$$u' = \frac{dI}{dt} \quad v' = \frac{d\omega_j}{dt}$$

Problems

13.

a.



$$\vec{r} = \frac{l}{2} \cos \theta \hat{x} + \frac{l}{2} \sin \theta \hat{y}$$

$$\dot{\vec{r}} = \frac{l}{2} \dot{\theta} \sin \theta \hat{x} - \frac{l}{2} \dot{\theta} \cos \theta \hat{y}$$

$$T_{cm} = \frac{m}{2} \dot{r}^2 = \frac{m}{2} \left(\frac{l}{2} \dot{\theta} \right)^2 = \frac{m l^2 \dot{\theta}^2}{8}$$

$$T_{rot} = \frac{1}{2} I \dot{\theta}^2$$

$$I = \int_{-l/2}^{l/2} \rho(r) \cdot r^2 dr = \int_{-l/2}^{l/2} m r^2 \cdot dr$$

$$= \frac{m}{3l} \cdot r^3 \Big|_{-l/2}^{l/2} = \frac{m}{3l} \left(\frac{l^3}{8} + \frac{l^3}{8} \right) = \frac{m l^2}{12}$$

(5.23)

$$T = T_{cm} + T_{rot} = \frac{m l^2 \dot{\theta}^2}{8} + \frac{m l^2 \dot{\theta}^2}{24} + \frac{m l^2 \dot{\theta}^2}{6}$$

Since this is the KE of one side total $T = \frac{m l^2 \dot{\theta}^2}{3}$

$$V = 2 \cdot m g \cdot \frac{l}{2} \sin \theta = m g l \sin \theta$$

$$m g l \sin(30) = \frac{m l^2 \dot{\theta}^2}{3}$$

$$\frac{3g}{2} = l \dot{\theta}^2$$

$$\dot{\theta} = \sqrt{\frac{3g}{2l}}$$

$$v = l \dot{\theta} = \sqrt{\frac{3gl}{2}}$$

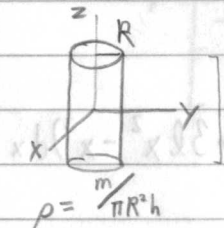
b. $\frac{d\theta}{dt} = \sqrt{\frac{3g}{2l}}$

$$d\theta = \sqrt{\frac{3g}{2l}} dt$$

$$\int_{\pi/6}^0 d\theta = \sqrt{\frac{3g}{2l}} t$$

$$t = \frac{\pi}{6} \sqrt{\frac{2l}{3g}}$$

14. For an inertia ellipsoid to be a sphere, $I_x = I_y = I_z$



$$I_x = I_y$$

$$I_z = \int_0^R \rho \cdot 2\pi r^3 dr$$

$$= \frac{m \cdot 2\pi h \cdot R^4}{4} = \frac{m R^2}{2}$$

(5.63)

$$I_x = \int_{-h/2}^{h/2} \int_{-R/2}^{R/2} (R^2/4 + z^2) dm$$

$$= \int_{-h/2}^{h/2} \left[\frac{m}{h} \left(\frac{R^2}{4} z + \frac{z^3}{3} \right) \right]_{-h/2}^{h/2} dz$$

$$= \frac{m}{h} \left[\frac{R^2 h}{4} + \frac{h^3}{24} \right]$$

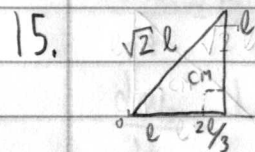
$$= m \frac{R^2}{4} + \frac{m h^2}{24}$$

$$\frac{m R^2}{4} + \frac{m h^2}{24} = \frac{m R^2}{2}$$

$$h^2 = 24 \cdot \frac{R^2}{4}$$

$$= 6 R^2$$

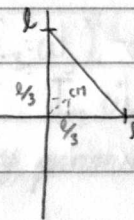
$$h = \sqrt{6} R$$



$$\rho = \frac{2M}{l^2}$$

$$x_{cm} = \frac{\int x dm}{M} = \frac{\int_0^l x^2 \rho dx}{M} = \frac{2M}{M} \cdot \frac{1}{3} \cdot l^3$$

$$= \frac{2l}{3}$$



Using the parallel-axis theorem

$$I_{cm} = I - m d^2$$

Since these are tensors, we want to figure out the inertia tensor of the figure on the left and the inertia tensor of a particle at the center of mass

$$I_{\alpha\beta} = \int_V \rho(\vec{r}) (\delta_{\alpha\beta} r^2 - r_\alpha r_\beta) dV \quad (5.23)$$

$$I_{11} = \rho \int_0^l \int_0^{l-x} y^2 dx dy$$

$$= \rho \int_0^l \int_0^{l-x} (l-x)^2 dx dy$$

$$= \rho \int_0^l l^2(l-x) - l(l-x)^2 + \frac{1}{3}(l-x)^3 dx$$

$$= \rho \int_0^l l^3 - l^2 x - l^3 + 2l^2 x - lx^2 + \frac{1}{3}(l^3 - 3l^2 x + 3lx^2 - x^3) dx$$

$$= \rho \int_0^l \frac{1}{3}(l^3 - x^3) dx$$

$$= \frac{\rho}{3} (l^4 - \frac{l^4}{4}) = \frac{\rho l^4}{4}$$

$$= \frac{M l^2}{2}$$

$$I_{22} = \rho \int_0^l \int_0^{l-x} x^2 dx dy$$

$$= \rho \int_0^l \frac{1}{3}(l-x)^3 dx = \frac{\rho}{3} \int_0^l (l^3 - 3xl^2 + 3x^2 l - x^3) dx$$

$$= \frac{\rho}{3} (l^4 - \frac{3}{2} l^4 + l^4 - \frac{l^4}{4})$$

$$= \frac{\rho}{3} (\frac{l^4}{4}) = \frac{M l^2}{6}$$

$$I_{33} = \rho \int_0^l \int_0^{l-x} x^2 + (l-x)^2 dx dy$$

$$= \rho \int_0^l \int_0^{l-x} l^2 - 2lx + 2x^2 dx dy$$

$$= \rho \int_0^l l^2(l-x) - l(l-x)^2 + \frac{2}{3}(l-x)^3 dx$$

$$= \rho \int_0^l (\frac{2}{3} l^3 - xl^2 + x^2 l - \frac{2}{3} x^3) dx$$

$$= \rho [\frac{2}{3} l^4 - \frac{1}{2} l^4 + \frac{1}{3} l^4 - \frac{2}{12} l^4] = \rho \cdot \frac{l^4}{3} = \frac{2M l^2}{3}$$

$$I_{12} = I_{21} = -\rho \int_0^l \int_0^{l-x} x(l-x) dx dy$$

$$= -\rho \int_0^l \frac{1}{2}(l-x)^2 - \frac{1}{3}(l-x)^3 dx$$

$$= -\rho \int_0^l (\frac{l^3}{6} - x^2 \frac{l}{2} + \frac{x^3}{3}) dx$$

$$= -\rho [\frac{1}{6} l^4 - \frac{1}{6} l^4 + \frac{1}{12} l^4]$$

$$= -\frac{M l^2}{6}$$

$$I = \begin{bmatrix} \frac{M l^2}{2} & -\frac{M l^2}{6} & 0 \\ -\frac{M l^2}{6} & \frac{M l^2}{6} & 0 \\ 0 & 0 & \frac{2M l^2}{3} \end{bmatrix}$$

In particle, $\rho = \delta(x - l/3) \delta(y - l/3)$

$$I_{11} = I_{22} = M \cdot x^2 = \frac{M l^2}{9}$$

$$I_{33} = M(x^2 + y^2) = \frac{2M l^2}{9}$$

$$I_{12} = I_{21} = -M(xy) = -\frac{M l^2}{9}$$

$$I = \begin{bmatrix} \frac{M l^2}{9} & -\frac{M l^2}{9} & 0 \\ -\frac{M l^2}{9} & \frac{M l^2}{9} & 0 \\ 0 & 0 & \frac{2M l^2}{9} \end{bmatrix}$$

$$I_{cm} - I_p = Ml^2 \begin{bmatrix} 7/18 & -5/18 & 0 \\ -5/18 & 1/18 & 0 \\ 0 & 0 & 16/18 \end{bmatrix}$$

$$= Ml^2/18 \begin{bmatrix} 7 & -5 & 0 \\ -5 & 1 & 0 \\ 0 & 0 & 16 \end{bmatrix}$$

$$\det(I_{cm} - \lambda I) = \det \begin{bmatrix} 7-\lambda & -5 & 0 \\ -5 & 1-\lambda & 0 \\ 0 & 0 & 16-\lambda \end{bmatrix}$$

$$= (7-\lambda)(1-\lambda)(16-\lambda) + 5(-5)(16-\lambda) = 0$$

$$= (16-\lambda)[(7-\lambda)(1-\lambda) - 25] = 0$$

$$= (16-\lambda)[7 - 8\lambda + \lambda^2 - 25] = 0$$

$$\lambda = 16, \frac{8 \pm \sqrt{64 - 72}}{2}$$

$$= 16, 4 \pm \sqrt{34}$$

16. $z = \frac{40x_1 + 50x_2 + 60x_3}{150}$

$$0 = \frac{40x_1 + 50x_2 + 60x_3 + 70x_4}{220}$$

$$300 = -70x_4$$

$$x_4 = -30/7$$

plane at $(-30/7, -30/7, -30/7)$

17.

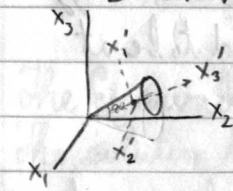


$$x_{cm} = \frac{\int x \, dm}{M} = \frac{\int_0^h x \cdot \rho \cdot \pi (x \tan \alpha)^2 \, dx}{\pi (h \tan \alpha)^2 \cdot \frac{1}{3} \rho}$$

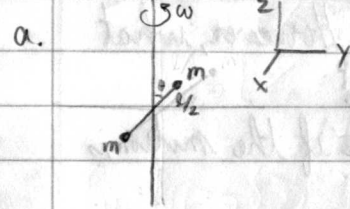
$$= \frac{1/4 \cdot h^4}{h^3/3} = 3h/4$$

$$T = T_{cm} + T_{rot}$$

$$= \frac{1}{2} M \cdot v_{cm}^2 + \frac{1}{2} I \omega^2$$



18



$$I_1 \dot{\omega}_1 - \omega_2 \omega_3 (I_2 - I_3) = N_1$$

$$I_2 \dot{\omega}_2 - \omega_3 \omega_1 (I_3 - I_1) = N_2$$

$$I_3 \dot{\omega}_3 - \omega_1 \omega_2 (I_1 - I_2) = N_3$$

$$\omega_1 = \dot{\theta} \sin \theta \sin \psi + \dot{\psi} \cos \theta$$

$$\omega_2 = \dot{\theta} \sin \theta \cos \psi - \dot{\psi} \sin \theta$$

$$\omega_3 = \dot{\theta} \cos \theta + \dot{\psi}$$

lim as sorry